Her A (3C 348) HST WFC3/UVIS Radio Interferometry F814W / Bill Cotton, NRAO

Basic radio interferometryEmphasis on VLBIImaging application

Simplest Radio Interferometer



Monochromatic, point source

Interferometer response

- Adding quarter wavelength to one arm allows measuring phase.
- Interferometer response is:

$$\rho = s^2 \ e^{-2\pi i\nu\tau}$$

Where

$$\tau = \frac{b}{c} \sin(\theta)$$

Interferometer response, cont'd

$$\rho = s^2 e^{-2\pi i \nu \frac{b}{c} \sin(\theta)}$$

substitute

$$u = \nu \frac{b}{c}$$
$$1 = sin(\theta)$$
$$B = s^{2}$$

Response becomes

$$\rho = B e^{-2\pi i \mathrm{ul}}$$

Extended Sources, limited FOV

Response linear, integrate over source (1D):

$$\rho_{\rm u} = \int B_l e^{-2\pi i {\rm ul}} {\rm dl}$$

This is a Fourier transform, trivially extended to 2D, Full 3D version is:

$$\rho_{\mathbf{u},\mathbf{v},\mathbf{w}} = \iint A_{l,m} B_{l,m} \ e^{-2j\pi \ (ul+vl+w(\sqrt{1-l^2-m^2}-1))} \ \frac{dl \ dm}{\sqrt{1-l^2-m^2}}$$

Which is not a Fourier transform.

Finite bandwidth

- In practice, real systems have finite bandwidth.
- Integral over ν τ will decorrelate signal when τ is large.
- Compensate by adding delays to align antennas.
- Measure multiple relative delays among antennas
- Delay and sky frequency related by Fourier transform, allows spectroscopy.

More realistic interferometer



Polarization

- Phase sensitive detectors respond to a single polarization state
- Two orthogonal polarizations are needed to fully sample wavefront.
 - Right and left hand circular polarization
 - Orthogonal linear polarization
- All four correlation products to fully measure polarization.

Circular feeds, 1st order

$$V_{RR} = I + V$$

$$V_{LL} = I - V$$

$$V_{RL} = I(d_{R,i} + d^*_{L,k}) - (jQ - U)e^{-j2\chi_m}$$

$$V_{LR} = I(d_{L,i} + d^*_{R,k}) - (jQ - U)e^{j2\chi_m}$$

I, Q, U, V = Stokes parameters, χ = parallactic angle d = "leakage" terms

Linear feeds, 1st order

$$V_{XX} = I + Q\cos 2\chi + U\sin 2\chi$$

$$V_{YY} = I - Q\cos 2\chi - U\sin 2\chi$$

$$V_{XY} = I(d_{X,i} + d^*_{Y,k}) - Q\cos 2\chi + U\sin 2\chi + jV$$

$$V_{YX} = I(d_{Y,i} + d^*_{X,k}) - Q\cos 2\chi + U\sin 2\chi - jV$$

I, Q, U, V = Stokes parameters, χ = parallactic angle d = "leakage" terms

Amplitude Calibration

 Need to calibrate visibility amplitudes into physical units, Janskys, for baseline i-k

$$\mathbf{V_{ik}^{obs}} = \rho_{\mathbf{jk}} \eta \sqrt{\frac{T_{S_j} T_{S_k}}{K_j K_k}}$$

 $\rho_{jk} = complex correlation coefficient$ $<math>\eta = efficiency factor$ $T_s = System temperature$ K = sensitivity in K/Jy

Full Calibration

Represent electric fields measured by the two detectors:

$$\mathbf{E} = \left(\begin{array}{c} e_p \\ e_q \end{array} \right)$$

Measured visibility is:

$$\mathbf{V_{ik}^{obs}} = \ (\mathbf{J_i} \otimes \mathbf{J_k^*}) (\mathbf{E_i} \otimes \mathbf{E_k^*})$$

Where $J = 2 \times 2$ complex "Jones" matrix, \otimes indicates outer product

Full Calibration, cont'd

Jones matrices are determined from observations of known calibrator sources and applied:

$$V^{cal}_{ik} \; = \; \left(J_i^{\;-1} \otimes {J^{-1}}^*_k \right) \, V^{obs}_{ik}.$$

Fringe Fitting

- Especially on long baselines instrumental delays may not be know a priori
 - Atmospheric delays
 - Instrumental delays
 - Clock errors
 - Errors in orbit

• Model phases as linear in time and frequency:

$$\phi_{t,\nu} = \phi_0 + \left(\frac{\partial \phi}{\partial \nu} \Delta \nu + \frac{\partial \phi}{\partial t} \Delta t\right)$$

• Fitting group delay and rate = "fringe fitting"

Time-Frequency data



Transformed to Delay - Rate



Interferometer arrays and imaging

- Single interferometer samples FT of sky brightness
- Many samples needed for good sampling of UV (Fourier) plane.
- Each pair of antennas gives a measurement
- FT of real function hermetian => conjugate points
- (n * n-1)/2 pair-wise combinations of n antennas.
- Point source response ("dirty beam") is the Fourier transform of u-v coverage.

VLA UV snapshot coverage and beam



U-V Coverage

Dirty Beam

Interferometer arrays and imaging, cont'd

- Interferometer parameters (u,v) vary with earth rotation.
- Improve coverage with time.

VLA 8 Hour Coverage and Beam



U-V Coverage

Dirty Beam

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Deconvolution

- Even very good uv coverage has holes
- Can use zero for unmeasured visibilities
- Allows inverting Fourier transform
- Derive "Dirty Image"
- Deconvolution to recover true sky distribution

Deconvolution, cont'd

Define Sampling Function:

$$S_{u,v} = \begin{cases} weight \text{ of sample where a sample was made} \\ 0 \text{ elsewhere.} \end{cases}$$

Sampled (calibrated) visibility:

$$V_{u,v}' = V_{u,v} S_{u,v}$$

which is defined everywhere,

Inverse Fourier transform of $V'_{u,v}$ gives "Dirty Image", $B'_{l,m}$ Inverse Fourier transform of $S_{u,v}$ gives "Dirty Beam", $D_{l,m}$

Deconvolution, cont'd

Convolution theorem says:

$$B_{l,m}' = B_{l,m} \star D_{l,m}$$

Where **★** indicates convolution

- Deconvolution needed to recover true sky brightness B_{1,m}
- Zeroes in S_{u,v} require nonlinear deconvolution

CLEAN Deconvolution variant



CLEAN of Noiseless Simulated Data



Dirty Image, 8 hr VLA

CLEAN deconvolved image contours 100 times lower

Weighting

 Weights in Sampling function, arbitrary, can be used to modify image

- "Uniform" weight \Rightarrow best resolution



Natural

Optimum, Robust=0



Self calibration

External calibration approximate

- Different time
- Different direction
- Phase calibration not practical for some VLBI
- If target is bright enough and model is available, it can be used as the calibrator
- Must be detectable in coherence time

Self calibration, cont'd

Most calibration errors affect antennas



Self calibration, cont'd

- For phase calibration have n-1 unknowns and n*(n-1)/2 measurements.
- Iterate calibration/imaging
 - Initial model uses external calibration if possible
 - VLBI initial point model usually good enough



Self calibration example



Thank you